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Stability of Networked Control Systems with Dynamic Controllers in the Feedback Loop

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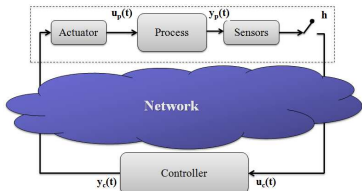
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- 1 Introduction
- 2 System Description
- 3 Stability Analysis
- 4 Numerical Examples
- 5 Conclusions and Future Work

Networked Control System



- Advantages

- Lower installation costs;
- Reduced system wiring;
- Greater flexibility;
- Higher reliability.

- Network-Induced Delay

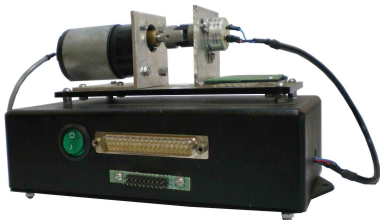
- Time-varying;

- Packet Loss

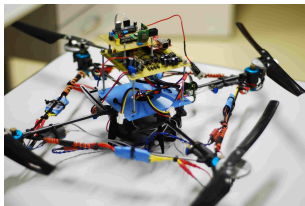
- Retransmitted or discarded;

Degrade system performance;
System instability.

- Control over sensor networks



- Unmanned aerial vehicles



- Remote surgery

Delay-dependent stability results for systems with delays

- Model transformations (see Fridman and Shaked (2001))
- Free-weighting matrices (see Wu *et al.* (2004));
- Jensen's inequality (see Gu *et al.* (2003), and Zhu and Yang (2008));

Pionner contribution (Halevi *et al.*, 1988);

One-channel feedback NCS × **Two-channel feedback NCS;**

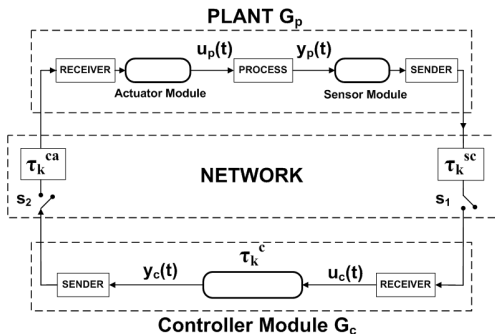
No packet loss × **Packet loss considered;**

Constant delays × **Time-varying delays;**

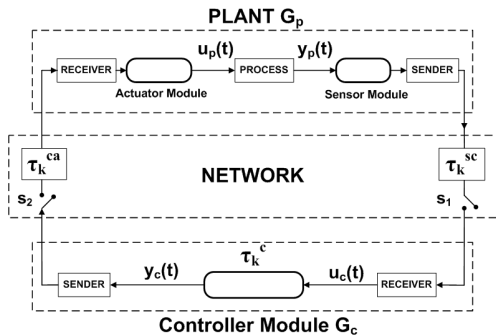
Only delay's upper bound considered × **Delay's lower and upper bounds;**

Delays derivative varying
with given bounds × **No restrictions are cast
upon the derivatives;**

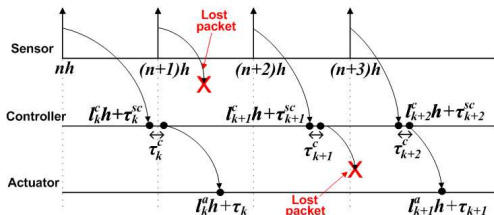
- 1 The new stability criterion presented here is able to deal with:
 - Dynamic controllers in the feedback loop;
 - Time-varying network delay;
 - Packet losses.
- 2 The theorem presented gives less conservative results compared with previous works for the network delay's upper bound.
- 3 It is also an extension of previous works that only consider proportional state feedback controllers in the stability analysis, being able to deal with a much larger set of control systems.



- 1 Closed-loop NCS with the possibility of dropping data and disordering;
- 2 Single packet transmission: all data lumped into one network packet;
- 3 Sensor module is *clock-driven* with sampling period h ;
- 4 Controller and actuator modules are *event-driven*;
- 5 Actuator uses the latest available control input.



- 1 τ_k^{sc} : delay from sensor to controller module for the k -th network packet;
- 2 τ_k^c : computation delay for the k -th network packet;
- 3 τ_k^{ca} : delay from controller to actuator module for the k -th network packet;
- 4 τ_k : total delay from sensor to actuator module for the k -th network packet.
- 5 The switches S_1 and S_2 model the possibility of packet loss.

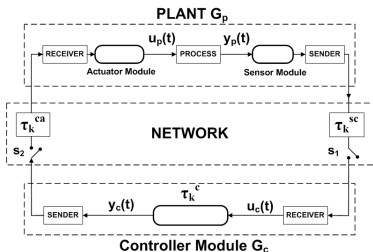


Remark

Dynamic controllers \rightarrow SC and CA channels considered separately.

Proportional controllers \rightarrow Only overall delay and package dropout considered.

- 1 Sensor module samples data at instants nh ;
- 2 l_k^c : index for the k -th packet received at the controller;
- 3 l_k^a : index for the k -th packet received at the actuator;
- 4 $\{l_1^c, \dots, l_n^c, \dots\} = \{1, \dots, n, \dots\}$
 \rightarrow no packet dropout or disordering from the sensor to the controller;
- 5 $\{l_1^a, \dots, l_n^a, \dots\} = \{l_1^c, \dots, l_n^c, \dots\}$
 \rightarrow no packet dropout or disordering occurred from the controller to the actuator;



- Delay constraints

$$\begin{aligned}
 (l_k^c - l_{k-1}^c)h + \tau_{\mathbf{k}}^{\text{sc}} &\leq \eta_1, \\
 (l_k^a - l_{k-1}^a)h + (\tau_{\mathbf{k}}^{\text{c}} + \tau_{\mathbf{k}}^{\text{ca}}) &\leq \eta_2, \\
 (l_k^a - l_{k-1}^a)h + \tau_{\mathbf{k}} &\leq \eta_3, \\
 \tau_1 &\leq \tau_{\mathbf{k}}^{\text{sc}}, \quad \tau_2 \leq \tau_{\mathbf{k}}^{\text{c}} + \tau_{\mathbf{k}}^{\text{ca}}, \quad \tau_3 \leq \tau_{\mathbf{k}}, \forall k \in \mathbb{N}^*.
 \end{aligned}$$

- Plant's model

$$\begin{aligned}
 \dot{x}_p(t) &= A_p x_p(t) + B_p u_p(t), \\
 y_p(t) &= C_p x_p(t),
 \end{aligned}$$

- Controller's model

$$\begin{aligned}
 \dot{x}_c(t) &= A_c x_c(t) + B_c u_c(t), \\
 y_c(t) &= C_c x_c(t - \tau_k^c) + D_c u_c(t - \tau_k^c),
 \end{aligned}$$

- Controller's input

$$\begin{aligned}
 u_c(t) &= y_p(l_k^c h) = C_p x_p(l_k^c h), \\
 \forall k \in \mathbb{N}^*, t \in [l_k^c h + \tau_k^{\text{sc}}, l_{k+1}^c h + \tau_{k+1}^{\text{sc}})
 \end{aligned}$$

- Plant's input

$$\begin{aligned}
 u_p(t) &= y_c(l_k^a h + \tau_k^{\text{sc}} + \tau_k^{\text{c}}) \\
 &= C_c x_c(l_k^a h + \tau_k^{\text{sc}}) + D_c C_p x_p(l_k^a h) \\
 \forall k \in \mathbb{N}^*, \tau_k &= \tau_k^{\text{sc}} + \tau_k^{\text{c}} + \tau_k^{\text{ca}}, \\
 t \in [l_k^a h + \tau_k, l_{k+1}^a h + \tau_{k+1}).
 \end{aligned}$$

- Defining $x(t) = [x_p^T(t), x_c^T(t)]^T \in \mathbb{R}^{n_p+n_c}$, the closed loop NCS can be described as:

$$\dot{x}(t) = Ax(t) + Bx(t - d_1(t)) + Cx(t - d_2(t)) + Dx(t - d_3(t)),$$

$$x(t) = \phi(t), t \in [t_1 - \eta_3, t_1],$$

with

$$\tau_j \leq d_j(t) \leq \eta_j, j \in \{1, 2, 3\},$$

$$\dot{d}_1(t) = 1, t \in [l_k^c h + \tau_k^{sc}, l_{k+1}^c h + \tau_{k+1}^{sc}),$$

$$\dot{d}_2(t) = \dot{d}_3(t) = 1, t \in [l_k^a h + \tau_k, l_{k+1}^a h + \tau_{k+1}),$$

$$A = \begin{bmatrix} A_p & 0 \\ 0 & A_c \end{bmatrix}, B = \begin{bmatrix} 0 & 0 \\ B_c C_p & 0 \end{bmatrix},$$

$$C = \begin{bmatrix} 0 & B_p C_c \\ 0 & 0 \end{bmatrix}, D = \begin{bmatrix} B_p D_c C_p & 0 \\ 0 & 0 \end{bmatrix}$$

$$d_1(t) = t - l_k^c h, t \in [l_k^c h + \tau_k^{sc}, l_{k+1}^c h + \tau_{k+1}^{sc}),$$

$$d_2(t) = t - l_k^a h - \tau_k^{sc}, t \in [l_k^a h + \tau_k, l_{k+1}^a h + \tau_{k+1}),$$

$$d_3(t) = t - l_k^a h, t \in [l_k^a h + \tau_k, l_{k+1}^a h + \tau_{k+1}).$$

Lyapunov function candidate

Considering the Lyapunov function candidate

$$V(t) = \sum_{i=1}^6 V_i(t),$$

where

$$\begin{aligned} V_1(t) &= x^T(t)Px(t), & V_2(t) &= \sum_{i=1}^3 \int_{t-\tau_i}^t [x^T(s)M_i x(s)] ds, \\ V_3(t) &= \sum_{i=1}^3 \int_{t-\eta_i}^t [x^T(s)N_i x(s)] ds, & V_4(t) &= \sum_{i=1}^3 \int_{t-\alpha_i d_i(t)}^t [x^T(s)Q_i x(s)] ds, \\ V_5(t) &= \sum_{i=1}^3 \int_{-\eta_i}^0 \int_{t+\beta}^t [\dot{x}^T(s)S_i \dot{x}(s)] ds d\beta, & V_6(t) &= \sum_{i=1}^3 \int_{-\tau_i}^0 \int_{t+\beta}^t [\dot{x}^T(s)Z_i \dot{x}(s)] ds d\beta, \end{aligned}$$

and matrices $P = P^T > 0$, $Q_j = Q_j^T \geq 0$, $M_j = M_j^T \geq 0$, $N_j = N_j^T \geq 0$, $Z_j = Z_j^T > 0$, $S_j = S_j^T > 0$, $j \in \{1, 2, 3\}$, the following stability criterion was derived.

Theorem 1

For given scalars $0 \leq \tau_i < \eta_i$ and $0 < \alpha_i < 1$, $i \in \{1, 2, 3\}$, the NCS previously described is asymptotically stable if there exist matrices $P = P^T > 0$, $Q_j = Q_j^T \geq 0$, $M_j = M_j^T \geq 0$, $N_j = N_j^T \geq 0$, $Z_j = Z_j^T > 0$, $S_j = S_j^T > 0$, $j \in \{1, 2, 3\}$, such that

$$\Omega = \begin{bmatrix} \Omega_{1,1} & \Omega_{1,2} & \Omega_{1,3} & \Omega_{1,4} & 0 & 0 & 0 & 0 & 0 & \frac{S_1}{\alpha_1 \eta_1} & \frac{S_2}{\alpha_2 \eta_2} & \frac{S_3}{\alpha_3 \eta_3} \\ * & \Omega_{2,2} & \Omega_{2,3} & \Omega_{2,4} & \frac{Z_1}{\eta_1 - \tau_1} & 0 & 0 & \Omega_{2,8} & 0 & \frac{S_1}{(1-\alpha_1)\eta_1} & 0 & 0 \\ * & * & \Omega_{3,3} & \Omega_{3,4} & 0 & \frac{Z_2}{\eta_2 - \tau_2} & 0 & 0 & \Omega_{3,9} & 0 & \frac{S_2}{(1-\alpha_2)\eta_2} & 0 \\ * & * & * & \Omega_{4,4} & 0 & 0 & \frac{Z_3}{\eta_3 - \tau_3} & 0 & \Omega_{4,10} & 0 & 0 & \frac{S_3}{(1-\alpha_3)\eta_3} \\ * & * & * & * & \Omega_{5,5} & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ * & * & * & * & * & \Omega_{6,6} & 0 & 0 & 0 & 0 & 0 & 0 \\ * & * & * & * & * & * & \Omega_{7,7} & 0 & 0 & 0 & 0 & 0 \\ * & * & * & * & * & * & * & \Omega_{8,8} & 0 & 0 & 0 & 0 \\ * & * & * & * & * & * & * & * & \Omega_{9,9} & 0 & 0 & 0 \\ * & * & * & * & * & * & * & * & * & \Omega_{10,10} & 0 & 0 \\ * & * & * & * & * & * & * & * & * & * & \Omega_{11,11} & 0 \\ * & * & * & * & * & * & * & * & * & * & * & \Omega_{12,12} & 0 \\ * & * & * & * & * & * & * & * & * & * & * & * & \Omega_{13,13} \end{bmatrix} < 0$$

holds, where

$$U_1 = \begin{bmatrix} 3 \\ \sum_{i=1}^3 \eta_i S_i \end{bmatrix}, U_2 = \begin{bmatrix} 3 \\ \sum_{i=1}^3 (\eta_i - \tau_i) Z_i \end{bmatrix},$$

$$U_3 = \sum_{i=1}^3 \left(M_i + N_i + Q_i - \frac{1}{\alpha_i \eta_i} S_i \right),$$

$$V_i = \left(\frac{1}{(1-\alpha_i)\eta_i} + \frac{1}{\eta_i - \tau_i} \right) S_i, i \in \{1, 2, 3\},$$

$$W_i = (1-\alpha_i)Q_i + \left(\frac{1}{\alpha_i \eta_i} + \frac{1}{(1-\alpha_i)\eta_i} \right) S_i, i \in \{1, 2, 3\},$$

$$\Omega_{1,1} = A^T P + PA + U_3 + A^T (U_1 + U_2) A,$$

$$\Omega_{1,2} = PB + A^T (U_1 + U_2) B,$$

$$\Omega_{1,3} = PC + A^T (U_1 + U_2) C,$$

$$\Omega_{1,4} = PD + A^T (U_1 + U_2) D,$$

$$\Omega_{2,2} = B^T (U_1 + U_2) B - V_1 - \frac{2}{\eta_1 - \tau_1} Z_1,$$

$$\Omega_{2,3} = B^T (U_1 + U_2) C,$$

$$\Omega_{2,4} = B^T (U_1 + U_2) D,$$

$$\Omega_{2,8} = \frac{1}{\eta_1 - \tau_1} (S_1 + Z_1),$$

$$\Omega_{3,3} = C^T (U_1 + U_2) C - V_2 - \frac{2}{\eta_2 - \tau_2} Z_2,$$

$$\Omega_{3,4} = C^T (U_1 + U_2) D,$$

$$\Omega_{3,9} = \frac{1}{\eta_2 - \tau_2} (S_2 + Z_2),$$

$$\Omega_{4,4} = D^T (U_1 + U_2) D - V_3 - \frac{2}{\eta_3 - \tau_3} Z_3,$$

$$\Omega_{4,10} = \frac{1}{\eta_3 - \tau_3} (S_3 + Z_3),$$

$$\Omega_{5,5} = -M_1 - \frac{1}{\eta_1 - \tau_1} Z_1,$$

$$\Omega_{6,6} = -M_2 - \frac{1}{\eta_2 - \tau_2} Z_2,$$

$$\Omega_{7,7} = -M_3 - \frac{1}{\eta_3 - \tau_3} Z_3,$$

$$\Omega_{8,8} = -N_1 - \frac{1}{\eta_1 - \tau_1} (S_1 + Z_1),$$

$$\Omega_{9,9} = -N_2 - \frac{1}{\eta_2 - \tau_2} (S_2 + Z_2),$$

$$\Omega_{10,10} = -N_3 - \frac{1}{\eta_3 - \tau_3} (S_3 + Z_3),$$

$$\Omega_{11,11} = -W_1, \quad \Omega_{12,12} = -W_2, \quad \Omega_{13,13} = -W_3.$$

What is the maximum delay that we guarantee will keep the system stable?

- $u_p(t) = Kx_p(l_k^a h) \rightarrow$ Proportional state-feedback controller

Same NCS example presented in Zhang *et al.* (2001)

$$A = \begin{bmatrix} 0 & 1 \\ 0 & -0.1 \end{bmatrix}, \quad B=0, \quad C=0, \quad D = \begin{bmatrix} 0 & 0 \\ -0.375 & -1.15 \end{bmatrix}.$$

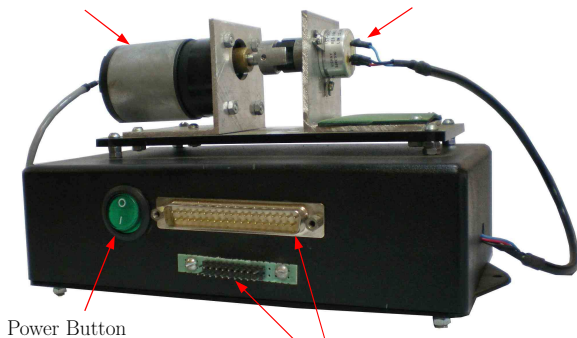
Table 1: Maximum delay's upper bounds for different criteria.

	η
Zhang <i>et al.</i> (2001)	0.45ms
Park <i>et al.</i> (2002)	53.8ms
Yue <i>et al.</i> (2004)	869.5ms
Naghshtabrizi <i>et al.</i> (2009)	870ms
Yue <i>et al.</i> (2005)	887.1ms
Theorem 1 ^a , Zhu <i>et al.</i> (2008)	1008ms

^aChoosing $\alpha_1=\alpha_2=0$, $\alpha_3=0.75$, $\tau_1=\tau_2=\tau_3=0$ s and $\eta_1=\eta_2=\frac{\eta_3}{2}$.

Brushed DC Motor

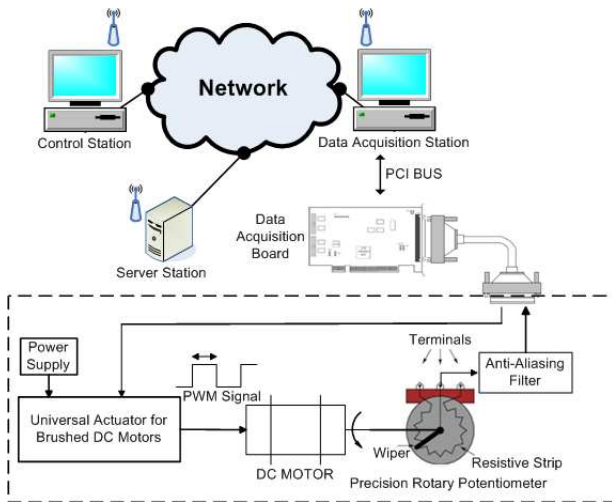
Rotary Potentiometer



Power Button

Connectors to the DAB

Numerical Examples 2



What is the maximum delay (η_3) that we guarantee will keep the system stable for a given delay lower bound (τ_3)?

PI Controller: $G_c(s) = K_p + \frac{1}{s}K_I$


$$\dot{x}(t) = Ax(t) + Bx(t - d_1(t)) + Cx(t - d_2(t)) + Dx(t - d_3(t))$$

$$A = \begin{bmatrix} A_p & 0 \\ 0 & A_c \end{bmatrix}, B = \begin{bmatrix} 0 & 0 \\ B_c C_p & 0 \end{bmatrix}, C = \begin{bmatrix} 0 & B_p C_c \end{bmatrix}, D = \begin{bmatrix} B_p D_c C_p & 0 \\ 0 & 0 \end{bmatrix}$$

$$A_p = \begin{bmatrix} 0 & 1 \\ 0 & -36.17 \end{bmatrix}, B_p = \begin{bmatrix} 0 \\ 36.3 \end{bmatrix}, C_p = \begin{bmatrix} 1 & 0 \end{bmatrix}, \\ A_c = 0, B_c = K_I = -47.45, C_c = 1, D_c = K_p = -11.86$$

Table 2: Maximum total delay boundary for different values of τ_3

τ_3	0s	20ms	40ms	50ms	68.5ms
η_3	59.85ms	61.63ms	64.34ms	65.79ms	68.58ms

^a Choosing $\tau_1 = \tau_2 = \frac{\tau_3}{2}$, $\eta_1 = \eta_2 = \frac{\eta_3}{2}$, $\alpha_1 = \alpha_2 = 0.5\alpha_3 = 0.375$. 

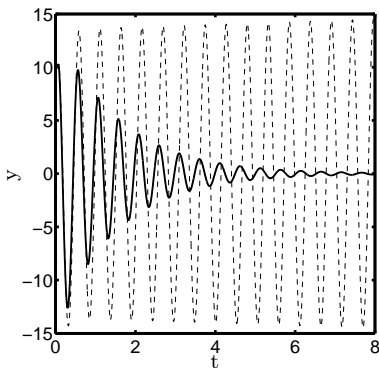


Figure 1: Simulation results using $\tau_3 = \eta_3 = 0.07s$ (solid) and $\tau_3 = \eta_3 = 0.078s$ (dashed).

Maximum total delay boundary for $\tau_3 \approx \eta_3$, obtained with Theorem 1, is **68.58** ms.

^a Choosing $\tau_1 = \tau_2 = \frac{\tau_3}{2}$, $\eta_1 = \eta_2 = \frac{\eta_3}{2}$, $\alpha_1 = \alpha_2 = 0.5\alpha_3 = 0.375$.

- ① Being able to deal with dynamic controllers in the feedback loop is this work's main contribution, since it extends previous works' results and allows the consideration of a much larger set of controllers;
- ② This work aids the analysis of many practical control systems that were not considered previous criteria. For example, the widely used PID controllers, which are very common in industrial environments, could not be modeled by those works;
- ③ The experimental apparatus shown and simulated here is already under testing and results about its stability will be published soon;
- ④ We are currently working on extending our previously published results in robust stability and stabilization of NCSs in order to deal with dynamic controllers.

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Questions?